

Artificial motion data for navigation sensors of a submarine running in periscope depth below wave surface

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- ❖ **Introduction**
 - ❖ **Equations of motion**
 - ❖ **Navigation data**
 - ❖ **Simulation**
 - ❖ **Conclusion**

Introduction

❖ Background

- Submarine navigation
 - GPS cannot be used.
 - IMU: Dead reckoning
 - Secondary navigational sensor: DVL, EM-Log, Depth gauge, etc.
- Development of navigation algorithm
 - Artificial data of navigation is necessary.
 - Especially the data during alignment near wave surface

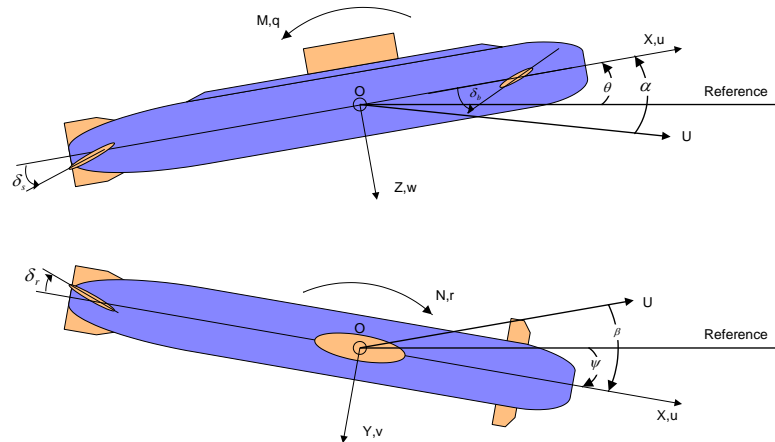
❖ Simulation program

- 6 DOF submarine motion for maneuvering
- Additional seakeeping motion during running or hovering near wave surface

Equations of motion

❖ Coordinate systems

- Earth-centered Earth-fixed: Reference and position
- NED: Position and Euler angle
- Body-fixed: Describe 6 DOF equations of motion



❖ State variables → Velocity and Displacement

- Linear and angular velocities
- Latitude, longitude, height, and Euler angles

Equations of motion

❖ 6 DOF equations of motion

$$m \left[\underline{v}^{b'} + \underline{\omega}_{nb}^b \times \underline{v}^b + \underline{\omega}_{nb}^{b'} \times \underline{r}_{-G}^b + \underline{\omega}_{nb}^b \times \left(\underline{\omega}_{nb}^b \times \underline{r}_{-G}^b \right) \right] = \underline{f}_{HD} + \underline{f}_{HS} + \underline{f}_G + \underline{f}_P + \underline{f}_\delta + \underline{f}_W + \underline{f}_C$$

$$I \underline{\omega}_{nb}^{b'} + \underline{\omega}_{nb}^b \times \left(I \underline{\omega}_{nb}^b \right) + m \underline{r}_{-G}^b \times \left(\underline{v}^{b'} + \underline{\omega}_{nb}^b \times \underline{v}^b \right) = \underline{m}_{HD} + \underline{m}_{HS} + \underline{m}_G + \underline{m}_P + \underline{m}_\delta + \underline{m}_W + \underline{m}_C$$

● External force

- HD, HS, G: Hydrodynamic, hydrostatic, and gravity
- P, δ : Propeller and control plane
- W, C: Wave and current

❖ Kinematic relations

$$\underline{v}^n = C_b^n \underline{v}^b, \quad \underline{\dot{\eta}} = D_b^n \underline{\omega}_{nb}^b$$

$$\dot{\Phi} = \frac{v_N}{R_m + h}, \quad \dot{\Theta} = \frac{v_E}{(R_t + h) \cos \phi}, \quad \dot{h} = -v_D$$

External force

❖ Hydrodynamic force

- Feldman model (1979, NSRDC)

$$X_{HD} = X_u \dot{u} + X(u) + X_{vr} vr + X_{wq} wq + X_{rp} rp + X_{vv} v^2 + X_{ww} w^2 + X_{qq} q^2 + X_{rr} r^2$$

$$Z_{HD} = Z_w \dot{w} + Z_q \dot{q} + Z_0 + Z_w w + Z_q q + Z_{vp} vp + Z_{|w|} |w| + Z_{ww} |w\sqrt{v^2 + w^2}|$$

$$+ \frac{\rho}{2} C_D \int_l b(x) w(x) \sqrt{w^2(x) + v^2(x)} dx + \frac{\rho}{2} L \bar{C}_L \int_{x_2}^{x_1} v(x) \bar{v}_{FW}(t - \tau[x]) dx$$

$$M_{HD} = M_w \dot{w} + M_q \dot{q} + M_0 + M_w w + M_q q + M_{rp} rp + M_{|w|} |w| + M_{ww} |w\sqrt{v^2 + w^2}| + M_{w|w|} w\sqrt{v^2 + w^2}$$

$$+ \frac{\rho}{2} C_D \int_l xb(x) w(x) \sqrt{w^2(x) + v^2(x)} dx + \frac{\rho}{2} L \bar{C}_L \int_{x_2}^{x_1} xv(x) \bar{v}_{FW}(t - \tau[x]) dx$$

❖ Propeller and control force

$$X_P = \rho n^2 D_P^4 K_T (J_P)$$

$$K_P = \rho n^2 D_P^5 K_Q (J_P)$$

$$X_\delta = X_{\delta_r} \delta_r^2 + X_{\delta_s} \delta_s^2 + X_{\delta_b} \delta_b^2$$

$$Z_\delta = Z_{\delta_s} \delta_s + Z_{\delta_b} \delta_b + Z_{\delta,\eta} \delta_s \left(\eta - \frac{1}{C} \right) C$$

$$M_\delta = M_{\delta_s} \delta_s + M_{\delta_b} \delta_b + M_{\delta,\eta} \delta_s \left(\eta - \frac{1}{C} \right) C$$

External force

❖ Hydrostatic and gravitational force

$$X_{HS} + X_G = -(W - B) \sin \theta$$

$$Z_{HS} + Z_G = (W - B) \cos \theta \cos \phi$$

$$M_{HS} + M_G = -(z_G W - z_B B) \sin \theta - (x_G W - x_B B) \cos \theta \cos \phi$$

❖ Wave effect

- Superpose wave induced acceleration to maneuvering one
 - Smooth change of motion value → Acceleration considered
 - Response amplitude operator and ITTC wave spectrum

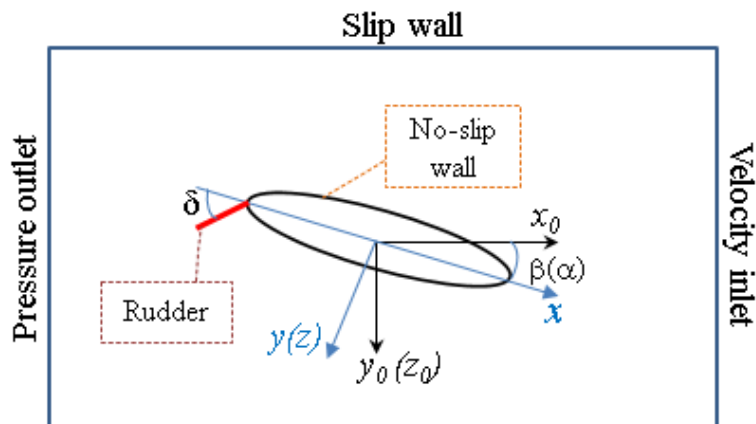
$$\dot{u}_w = -\sum_{i=1}^N \omega_i^2 RAO_{x_i} \zeta_i \cos \left[k_i (X \cos \alpha + Y \sin \alpha) - \omega_i t + \varepsilon_{x_i} + \delta_i \right]$$

$$\dot{w}_w = -\sum_{i=1}^N \omega_i^2 RAO_{z_i} \zeta_i \cos \left[k_i (X \cos \alpha + Y \sin \alpha) - \omega_i t + \varepsilon_{z_i} + \delta_i \right]$$

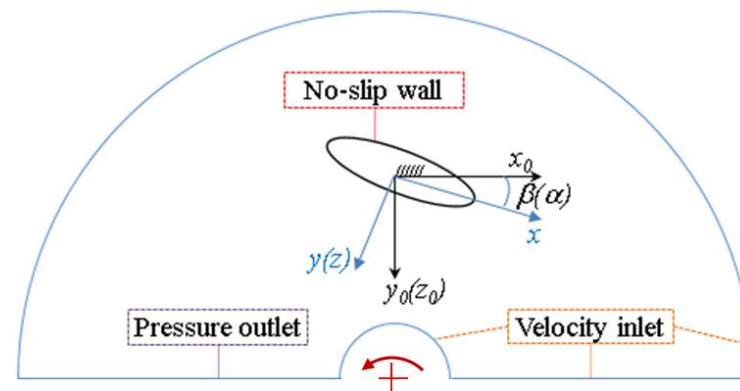
$$\dot{q}_w = -\sum_{i=1}^N \omega_i^2 RAO_{\theta_i} k_i \zeta_i \cos \left[k_i (X \cos \alpha + Y \sin \alpha) - \omega_i t + \varepsilon_{\theta_i} + \delta_i \right]$$

Hydrodynamic coefficient

❖ Numerical PMM test



Slip wall
Drift test

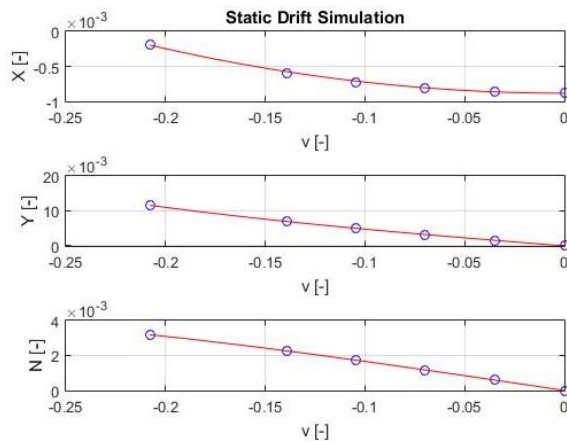


Rotating arm test

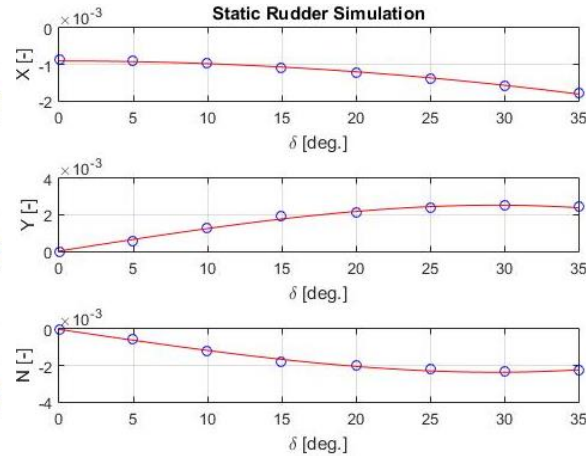
Test ↓	α [°] ↓	β [°] ↓	δ [°] ↓	r' ↓
Static drift ↓	0 ↓	2, 4, 6, 8, 12 ↓	0 ↓	0 ↓
Static angle of attack ↓	0, ±2, ±4, ±6, ±8 ↓	0 ↓	0 ↓	0 ↓
Static control plane ↓	0 ↓	0 ↓	0, 5, 10, 15, 20, 25, 30, 35 ↓	0 ↓
Turn ↓	0 ↓	0 ↓	0 ↓	0.12, 0.17, 0.21, 0.25, 0.29 ↓
Drift and turn ↓	0 ↓	±3, ±5, ±7, ±9 ↓	0 ↓	0.21, 0.25, 0.29 ↓
Angle of attack and turn ↓	3, 5, 7, 9 ↓	0 ↓	0 ↓	0.21, 0.25, 0.29 ↓

Hydrodynamic coefficient

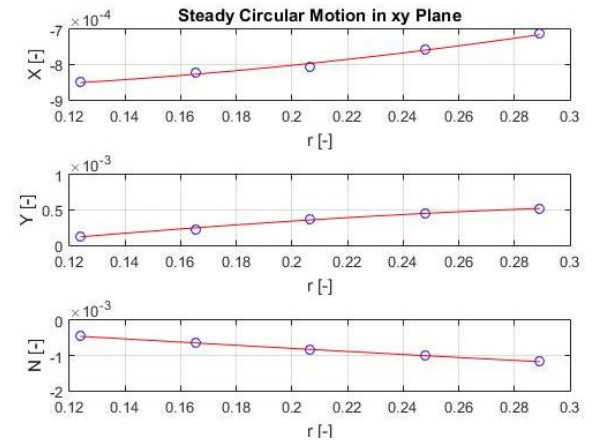
❖ Horizontal plane



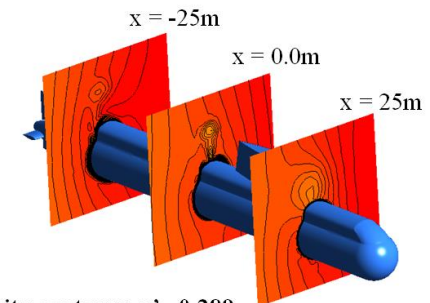
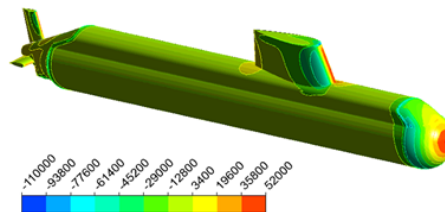
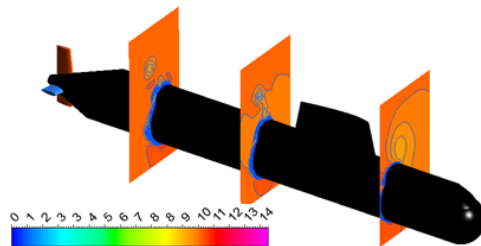
Static drift



Static rudder



Turning



Velocity contours, $r' = 0.289$

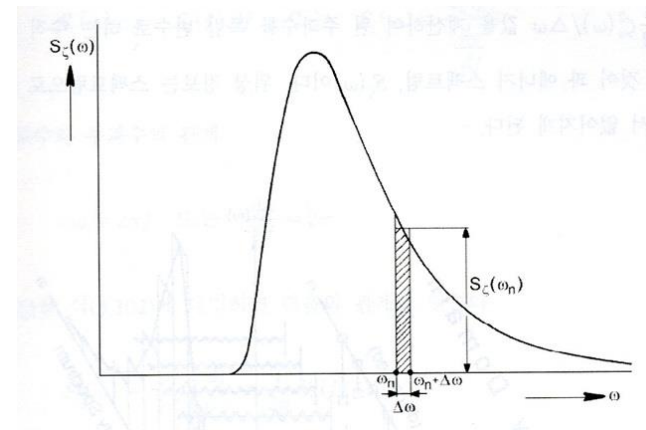
Wave effect

❖ RAO (Response Amplitude Operator)

- ANSYS AQWA (3D panel method based on potential theory)
- Pre-calculation and interpolation for speed and heading
 - Speed: 2~20 knots, 2 knots interval
 - Wave heading: 0~180 degrees, 45 degrees interval
 - Wave frequency: 0.2~3.0 rad/s → Long-crested irregular wave

❖ Wave

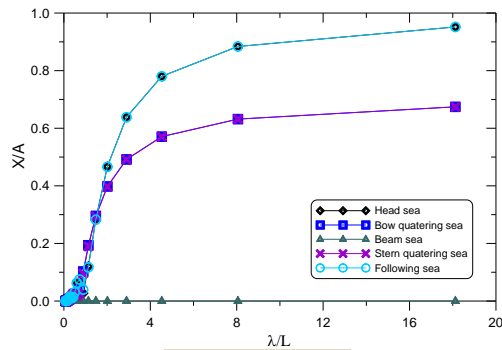
- Long-crested irregular wave
 - Superpose various regular waves
 - ITTC wave spectrum → Wave height
 - Random phase



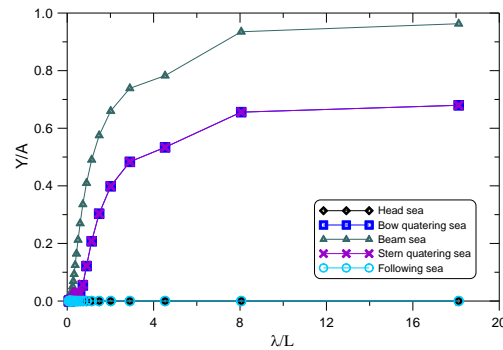
Wave effect

RAO

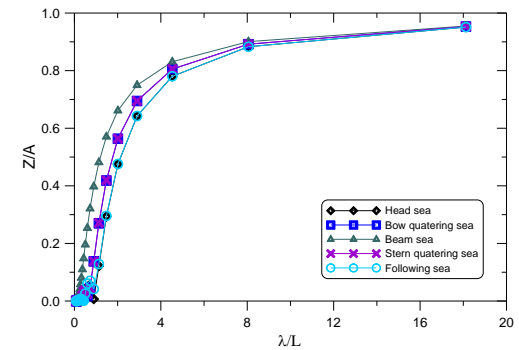
Stationary case



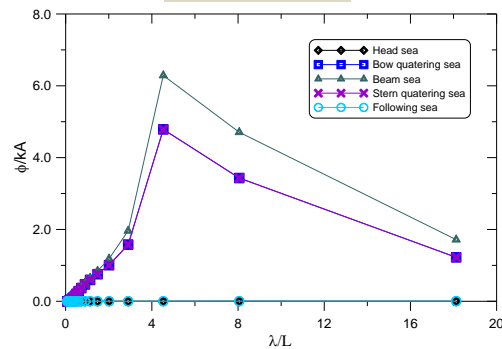
Surge



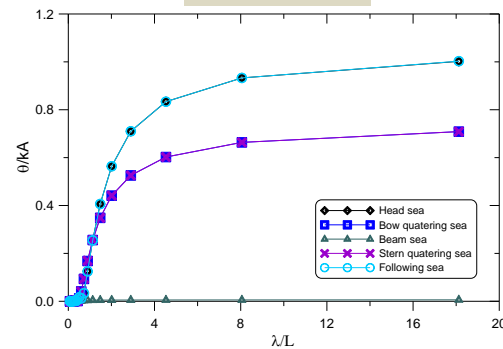
Sway



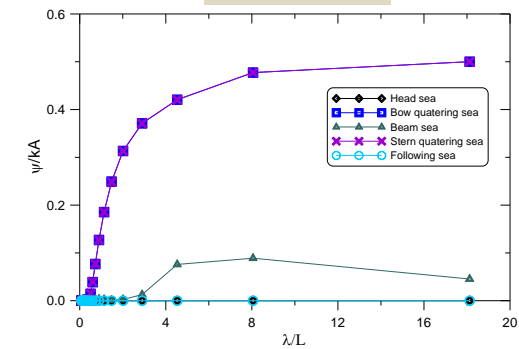
Heave



Roll



Pitch



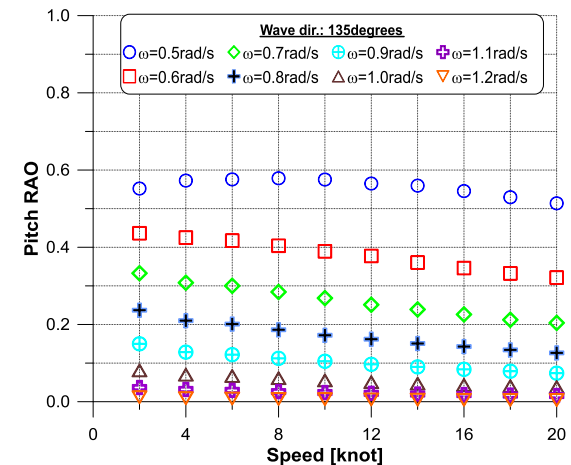
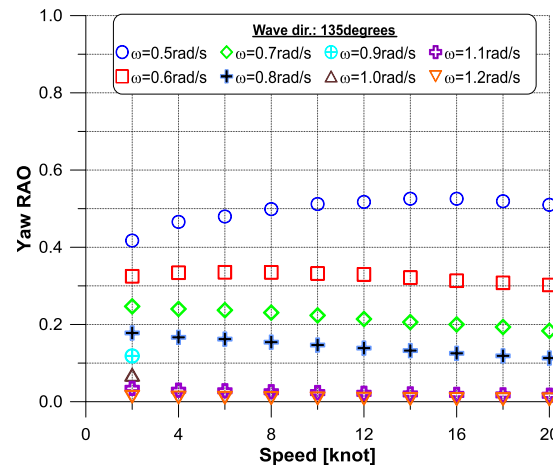
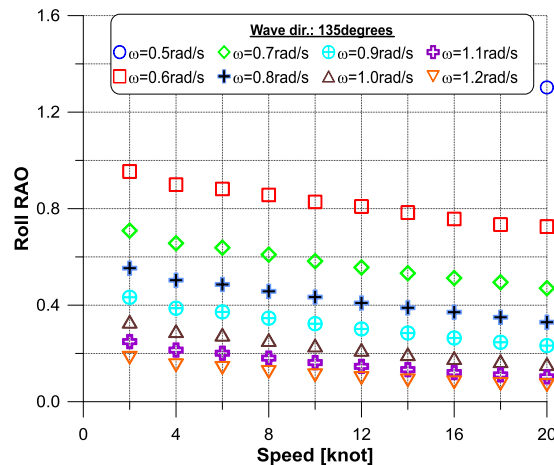
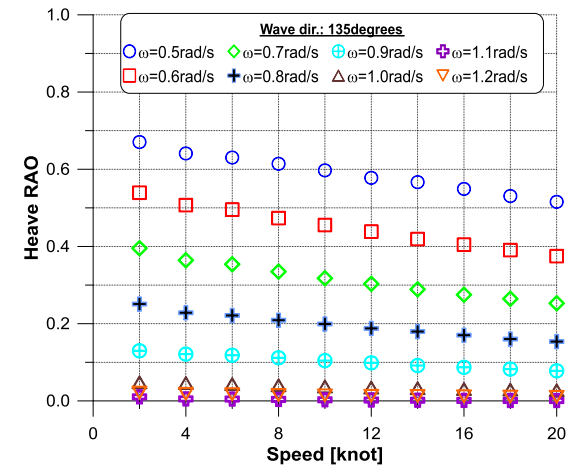
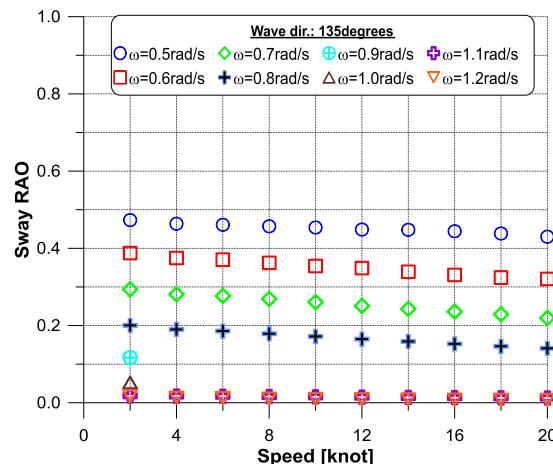
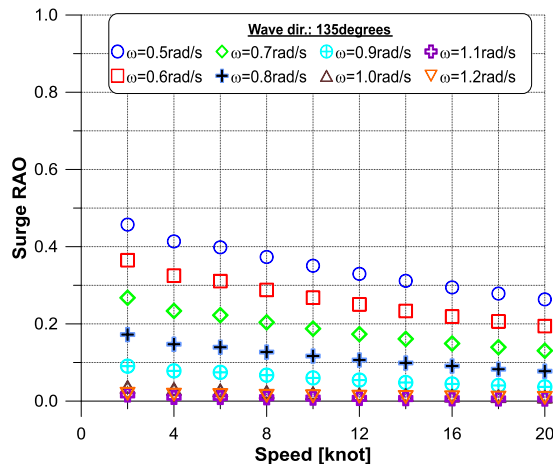
Yaw



Wave effect

❖ RAO (Beam sea)

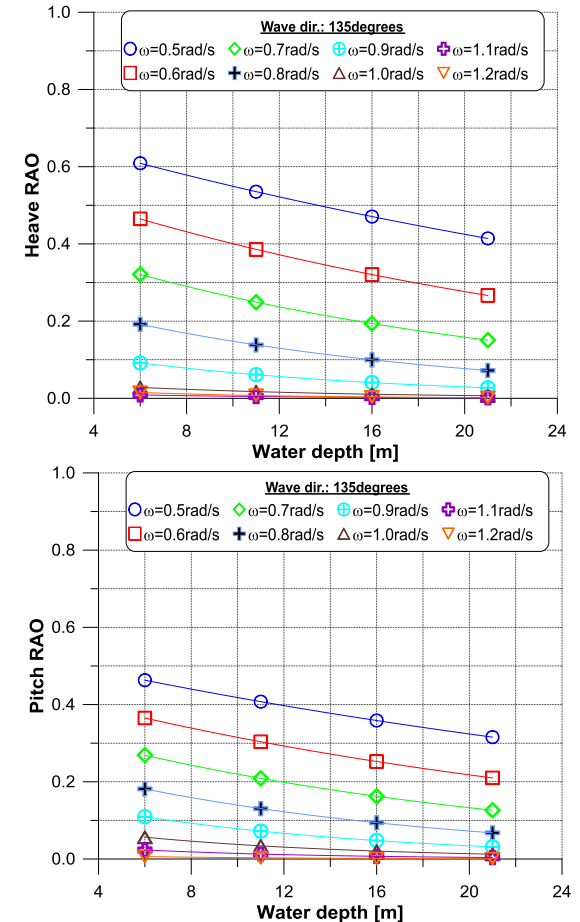
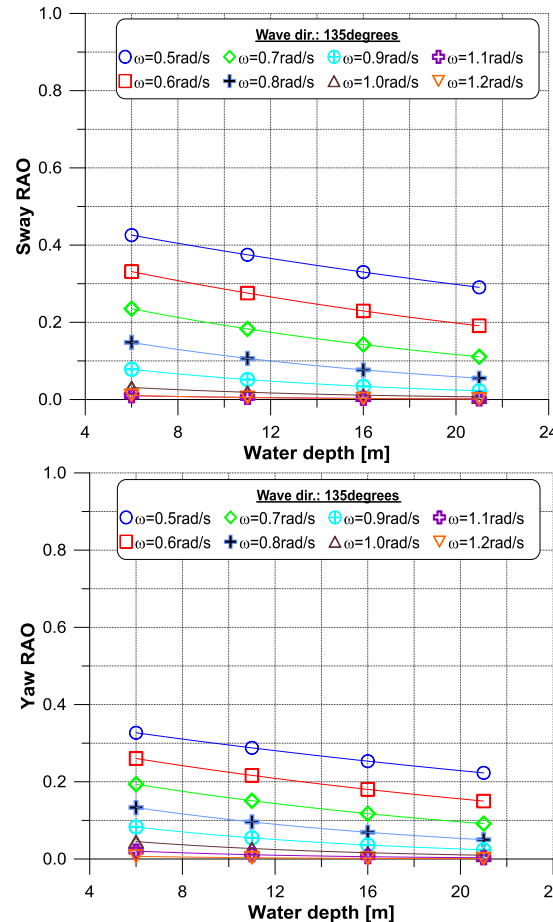
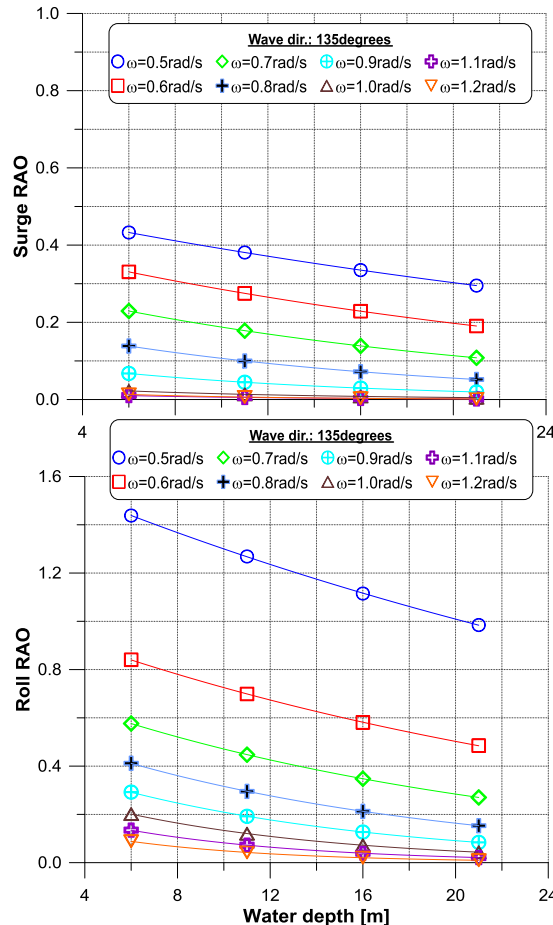
● Speed change



Wave effect

❖ RAO (Bow quartering sea)

- Depth change \rightarrow modeling using $\text{Exp}(-kz)$



Navigational data

❖ Data stored in navigation sensors

- Measured or calculated values
- Earth's rotation and curved surface effect included

Sensor	Item	Unit	Reference
INS	Position(Θ, Φ, h)	rad, m	Earth-fixed
	Velocity(v_N, v_E, v_D)	m/s	Earth-fixed
	Attitude(ϕ, θ, ψ)	rad	Earth and Body-fixed
	Angular rate($\omega_x, \omega_y, \omega_z$)	rad/s	Body-fixed
	Acceleration(a_x, a_y, a_z)	m/s ²	Body-fixed
DVL	Velocity(u_r, v_r, w_r)	m/s	Body-fixed
DM-Log	Forward speed(V)	m/s	Body-fixed
Depth gauge	Depth(-h)	m	Earth-fixed

Navigational data

❖ IMU (Gyro and accelerometer)

- Earth's rotation and curved surface effect (Transport rate)

$$\underline{\omega}_{ib}^b = \begin{bmatrix} \omega_x & \omega_y & \omega_z \end{bmatrix}^T = \underline{\omega}_{nb}^b + C_n^b \underline{\omega}_{in}^n, \quad \text{where, } \underline{\omega}_{in}^n = \underline{\omega}_{ie}^n + \underline{\omega}_{en}^n$$

$$\underline{a}^b = \begin{bmatrix} a_x & a_y & a_z \end{bmatrix}^T = C_n^b \left[\dot{\underline{v}}^n + \left(2\underline{\omega}_{ie}^n + \underline{\omega}_{en}^n \right) \times \underline{v}^n - \underline{g}^n \right]$$

$$\underline{\omega}_{ie}^n = \begin{bmatrix} \Omega_{ER} \cos \Phi & 0 & -\Omega_{ER} \sin \Phi \end{bmatrix}^T$$

$$\underline{\omega}_{en}^n = \begin{bmatrix} \frac{v_E}{R_t + h} & -\frac{v_N}{R_m + h} & -\frac{v_E \tan \Phi}{R_t + h} \end{bmatrix}^T$$

- Sensor position

$$\dot{\underline{v}}_s^b = \underline{v}'^b + \underline{\omega}_{nb}^b \times \underline{v}^b + \underline{\omega}'_{nb}^b \times \underline{r}_s^b + \underline{\omega}_{nb}^b \times \left(\underline{\omega}_{nb}^b \times \underline{r}_s^b \right)$$

❖ Noise effect

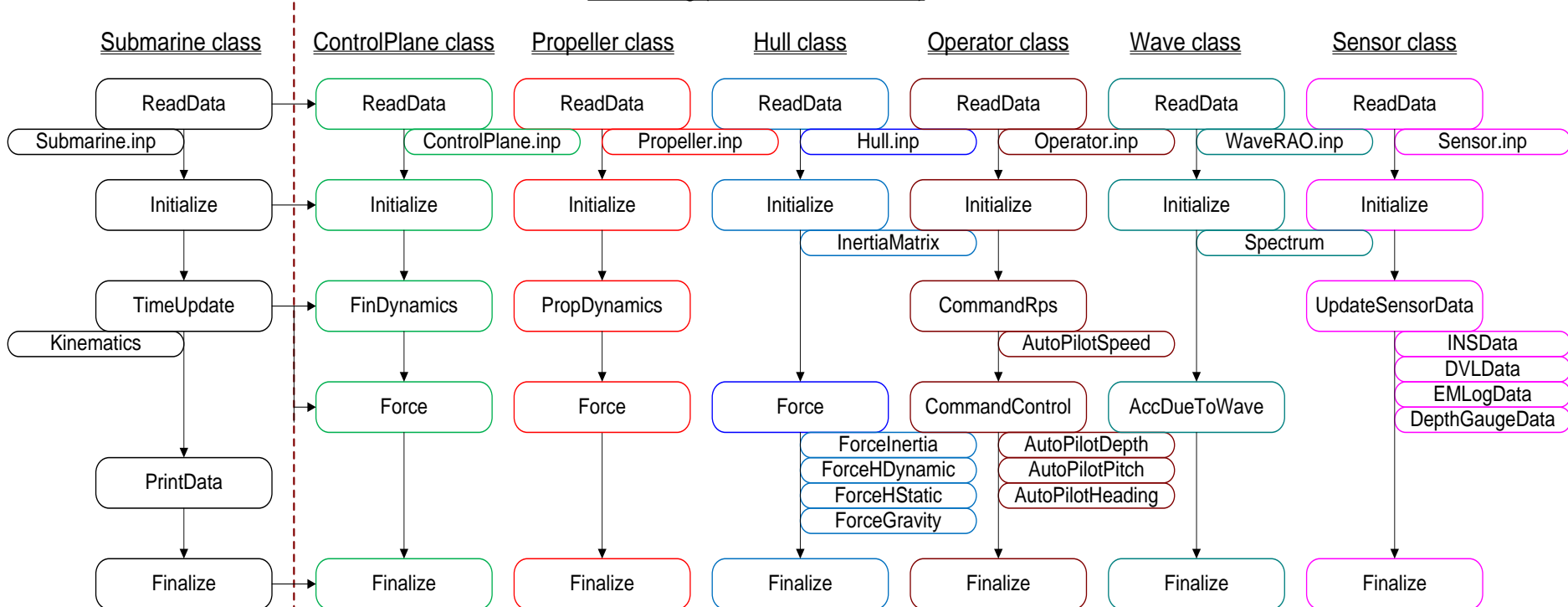
$$z = (1 + \varepsilon_{SF}) x + \varepsilon_{bias} + \varepsilon_{noise}$$

Simulation

❖ Computer program

- Visual Studio 2010 MFC based dialog program
- Main class: Submarine
- Subclass: Hull, Propeller, ControlPlane, Operator, Sensor, Wave

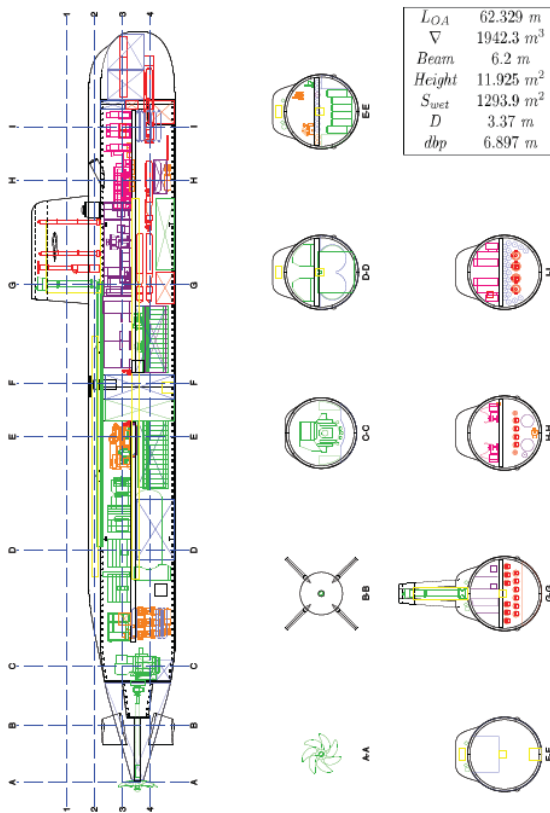
SubSimDlg (VS 2010, MFC based)



Simulation

❖ Sample submarine

- Thune, S., “Simulation of Submarine Manoeuvring”, Master thesis, Royal Institute of Technology, Sweden, 2015



L_{OA}	62.329 m
∇	1942.3 m ³
Beam	6.2 m
Height	11.925 m ²
S_{wet}	1293.9 m ²
D	3.37 m
dbp	6.897 m

x_G	= 0	[m]
y_G	= 0	[m]
z_G	= -0.36697	[m]
x_B	= 0	[m]
y_B	= 0	[m]
z_B	= -0.54848	[m]
k_{xx}	= 0.04176	[-]
k_{yy}	= 0.24012	[-]
k_{zz}	= 0.23858	[-]
k_{xy}	= 0.0010303	[-]
k_{zx}	= 0.031494	[-]
k_{yz}	= 0.0021967	[-]
S_1	= 1.17	[-]
S_2	= -1.281	[-]
x_1	= 10.825	[m]
x_{FW}	= 10.825	[m]
z_{FW}	= 0	[m]
β_{ST}	= 0.133	[rad]
x_{ap}	= -33.978	[m]

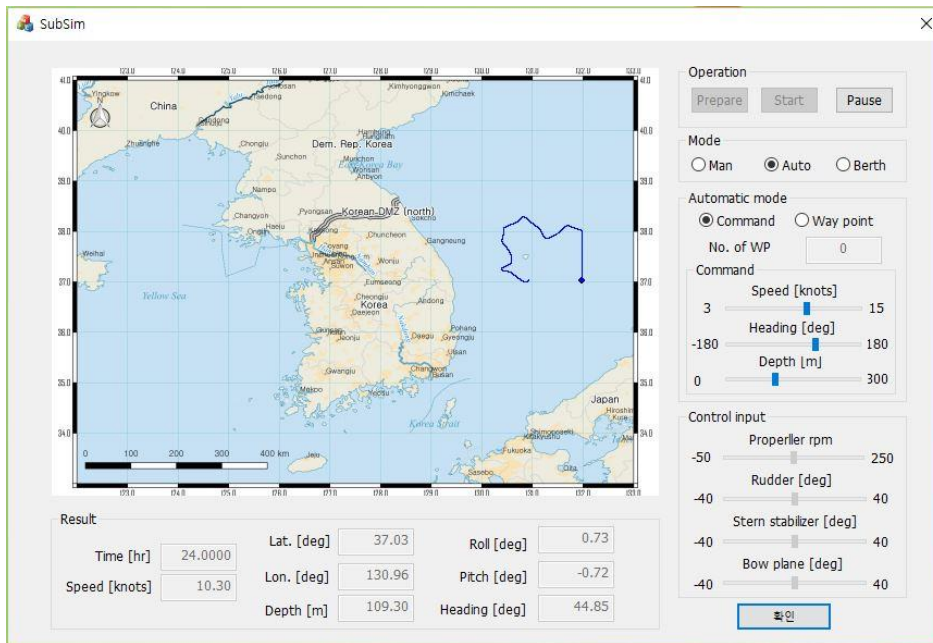
X		Y		Z	
$X'_{\dot{u}}$	= -0.00048129	$Y'_{\dot{p}}$	= -0.00049893	$Z'_{\dot{q}}$	= -0.00020374
$X'_{r\dot{p}}$	= 0.00049893	$Y'_{\dot{r}}$	= -0.0016656	$Z'_{\dot{w}}$	= -0.01334
$X'_{q\dot{q}}$	= 0.00080214	$Y'_{\dot{v}}$	= -0.01744	$Z'_{v\dot{p}}$	= -0.01744
$X'_{q q }$	= 0	$Y'_{\dot{p}}$	= -0.0012749	$Z'_{\dot{q}}$	= -0.0040505
X'_{rr}	= 0.001123	Y'_{pq}	= 0.00020374	$Z'_{q q }$	= 0
X'_{vr}	= 0.016132	Y'_{wp}	= 0.01334	Z'_{rr}	= 0
X'_{uu}	= -0.0011095	$Y'_{\dot{r}}$	= -0.00082411	Z'_{vr}	= 0
X'_{vv}	= 0.011293	$Y'_{r r }$	= 0	Z'_{vv}	= 0
X'_{ww}	= 0.0037018	$Y'_{v r }$	= 0	Z'_{vw}	= 0
$X'_{w w }$	= 0	$Y'_{ v r }$	= 0	$Z'_{\dot{w}}$	= -0.023841
X'_{wq}	= -0.012339	Y'_{wr}	= 0	$Z'_{ w }$	= 0
$X'_{w q }$	= 0	$Y'_{\dot{v}}$	= -0.061469	Z'_{ww}	= 0.0033377
$X'_{\delta_r \delta_r}$	= -0.0015181	$Y'_{v v }$	= -0.063314	$Z'_{w R}$	= 0
$X'_{\delta_r \delta_r \eta}$	= 0	Y'_{vw}	= 0	$Z'_{w q }$	= 0
X'_{δ_s}	= 0	$Y'_{\dot{r}}$	= 0.0034403	Z'_{wq}	= 0
$X'_{\delta_s \delta_s}$	= -0.0015181	$Y'_{\delta_r \delta_r }$	= 0	Z'_{δ_s}	= -0.0034403
$X'_{\delta_s \delta_s \eta}$	= 0	$Y'_{\delta_r \eta}$	= 0.00034403	$Z'_{\delta_s \delta_s }$	= 0
X'_{δ_b}	= 0	$Y'_{ r \delta_r}$	= 0	$Z'_{\delta_s \eta}$	= -0.00034403
$X'_{\delta_b \delta_b}$	= -0.0017798	Y'_{*}	= 0	$Z'_{ q \delta_s}$	= 0
$X'_{rr\dot{\xi}}$	= 0	$Y'_{r\dot{\xi}}$	= 0	Z'_{δ_b}	= -0.003852
$X'_{vv\dot{\xi}}$	= 0	$Y'_{v\dot{\xi}}$	= 0	$Z'_{\delta_b \delta_b }$	= 0
				Z'_{*}	= -0.00029985
				$Z'_{rr\dot{\xi}}$	= 0
				$Z'_{vv\dot{\xi}}$	= 0
				$Z'_{\dot{\xi}}$	= 0
				$Z'_{\dot{\xi} \theta }$	= 0



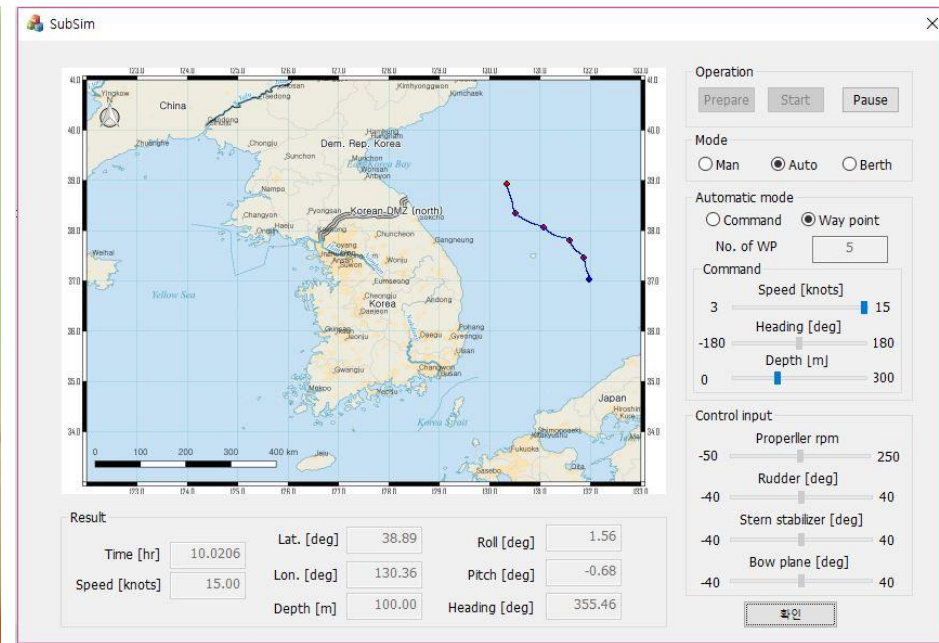
Simulation

❖ GUI to control a submarine

- Manual and automatic mode
 - Automatic mode: Command and way point



Command mode

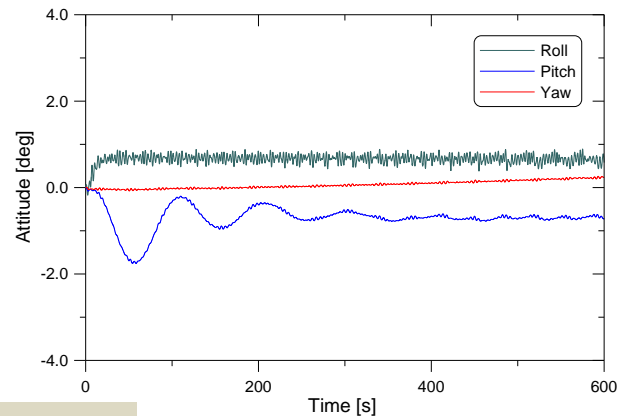
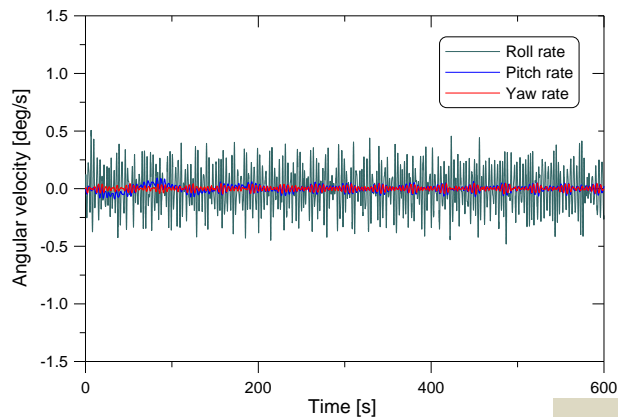


Way point mode

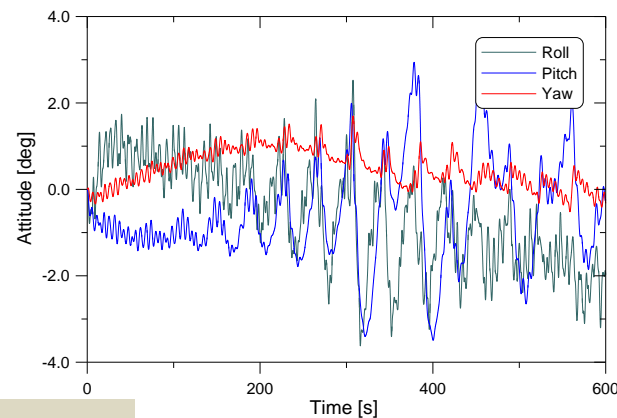
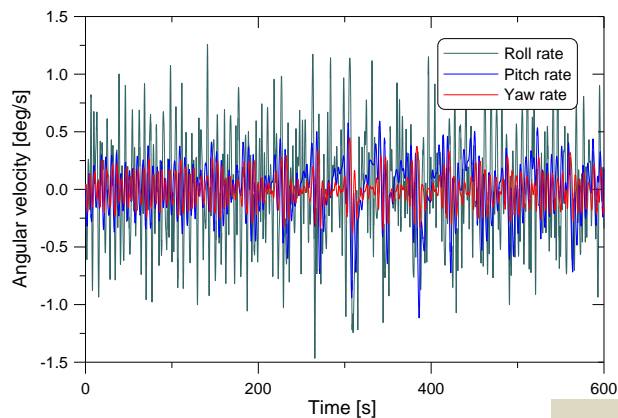
Simulation

❖ IMU data

● Angular velocity and attitude



Sea state 3



Sea state 4

Conclusion

❖ Submarine 6 DOF equations of motion

- Maneuvering motion based on Feldman model
- Wave effect added by RAO calculated by ANSYS AQWA
- Hydrodynamic coefficient and RAO
 - Numerical PMM test and RAO for various regular wave

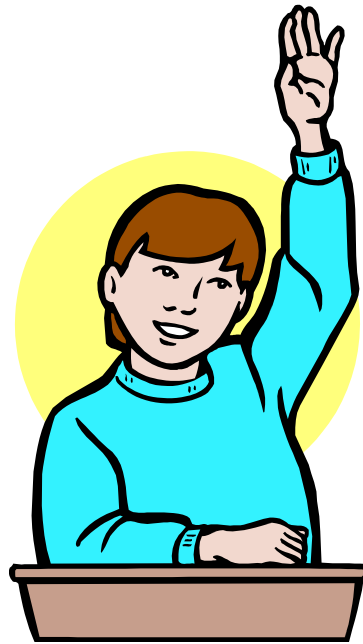
❖ Navigational data

- IMU data including Earth's rotation and transport rate

❖ Simulation

- MFC based GUI program to manage submarine motion
- Binary output data file for confirming navigational algorithm

Thank you for your kind attention



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