

# IMPROVING ACOUSTIC STEALTH

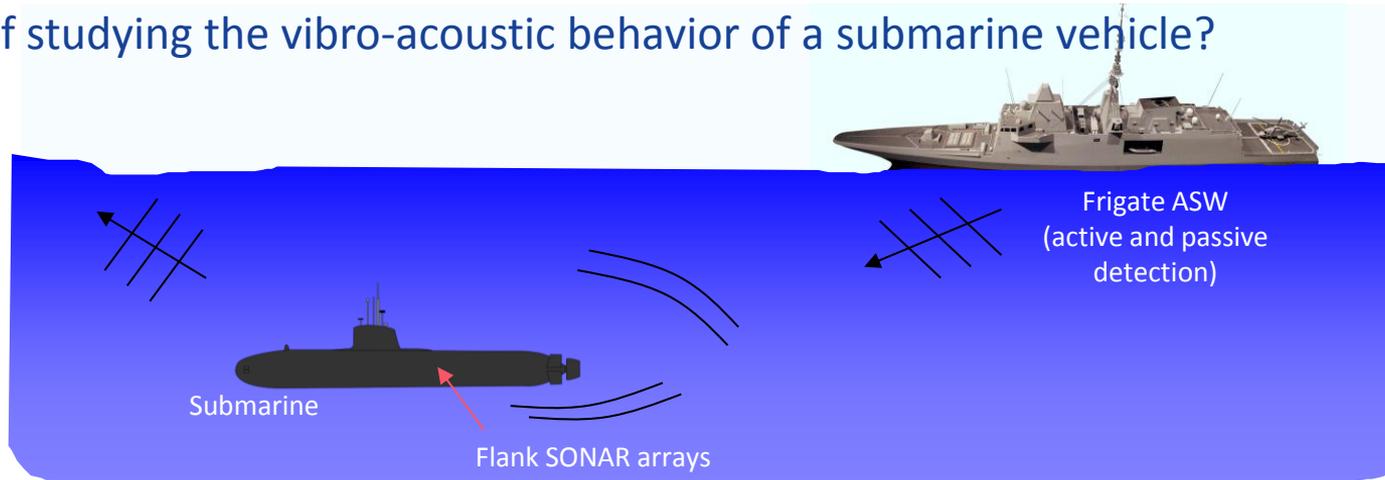
Analysis of the vibro-acoustic behavior of a submarine hull on a wide frequency range using experimental and numerical approaches

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## Interest of studying the vibro-acoustic behavior of a submarine vehicle?



Hull acoustic performances	Operational capability
Far-field radiated noise	Acoustic stealth
Reflection/scattering	Target strength
Self radiated noise	Sonar performances

Predict the vibro-acoustic behavior of a submerged shell and understand the physical phenomena,  
**before** its construction

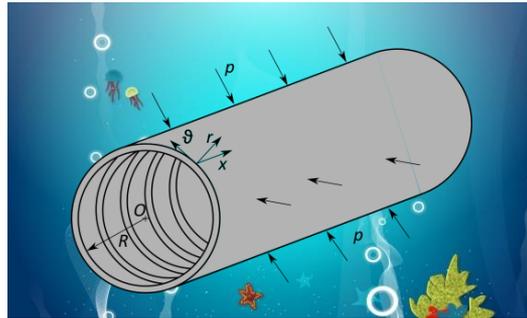
Development of  
numerical predictive tools

Experimental procedures

Improve the acoustic  
stealth of the vessels

# CURRENT CHALLENGES IN NUMERICAL MODELING

- SONAR is able to detect a noise source from a few Hz to dozens of kHz
  - Techniques to predict the vibro-acoustic response for a wide frequency range
  - Simplified model of a cylindrical shell submerged in an infinite fluid medium

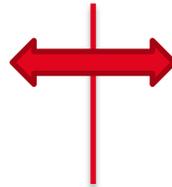


Low frequency range: FEM/BEM

- Structural complexity
- Calculation cost depends on mesh size

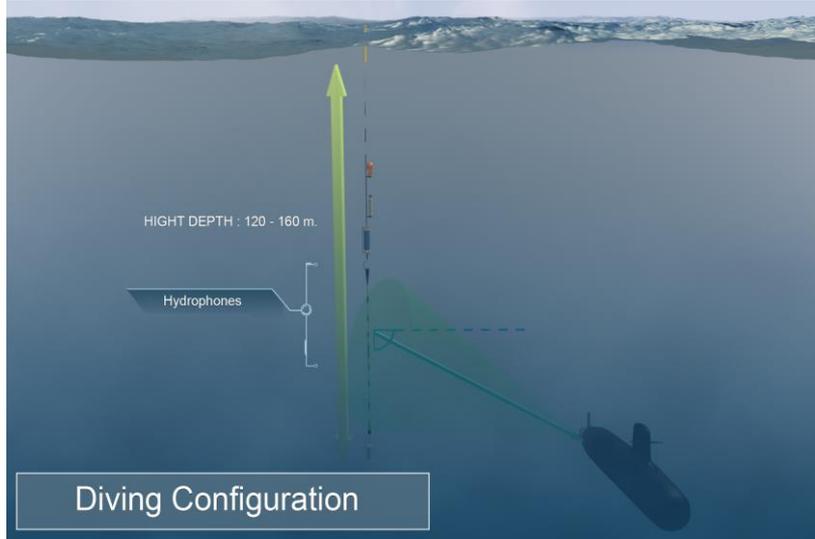
High frequency range: SEA

- Energy balance between subsystems
- Strong assumptions
- Only global results



How to model on a wide frequency range?

# CHALLENGES IN MEASUREMENTS



*Sketch of the MARS500@ hydrophone array*

Experiments at sea are:

- costly and time-consuming
- not ideal to understand the physical phenomena
- only when the submarine is built



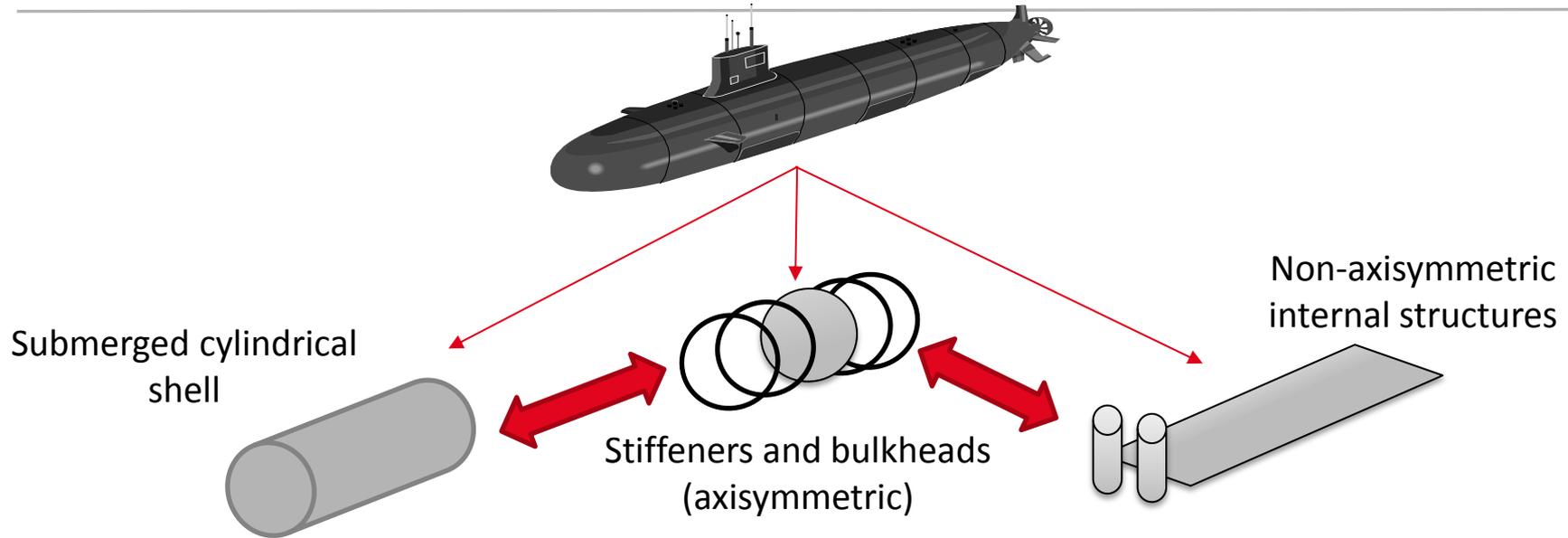
How can the vibro-acoustics of a stiffened shell be measured?

1. The CTF method
2. Experimental work
3. Results and Discussion
4. Summary

# ▼ 1. The CTF method

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# A SUB-STRUCTURING APPROACH:

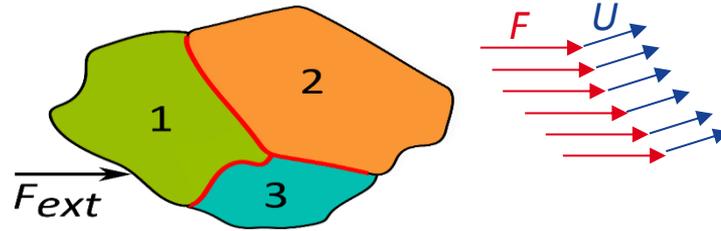


\*L. Maxit, J.-M. Ginoux, Prediction of the vibro-acoustic behavior of a submerged shell non periodically stiffened by internal frames, JASA 128(1):137-151, 2010.

\*\*V. Meyer, L. Maxit, J.-L. Guyader, T. Leissing, Prediction of the vibroacoustic behavior of a submerged shell with non-axisymmetric internal substructures by a condensed transfer function method, JSV, 360:260-276, 2016.

# PRINCIPLE OF THE CONDENSED TRANSFER FUNCTION METHOD

- Extension of the admittance method for line coupled systems:



$$\text{Mechanical admittance } Y = \frac{\text{displacement } U}{\text{force } F}$$

Solving the coupling forces between the subsystems:

$$[F_c] = ([Y_{ij}^1] + [Y_{ij}^2] + [Y_{ij}^3])^{-1} [\tilde{U}]$$

- Requires only characteristics from the uncoupled subsystems
- The admittances can be calculated by any method

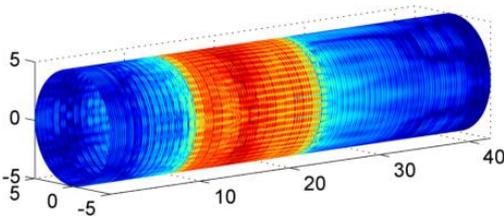
# THE CTF METHOD APPLIED TO STIFFENED SUBMERGER CYLINDRICAL SHELLS

Calculation of the admittances for each subsystem :

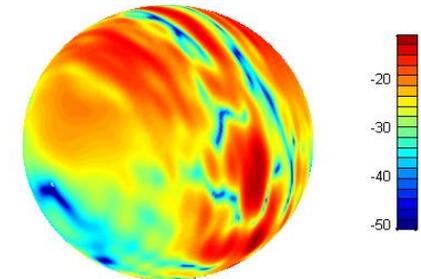
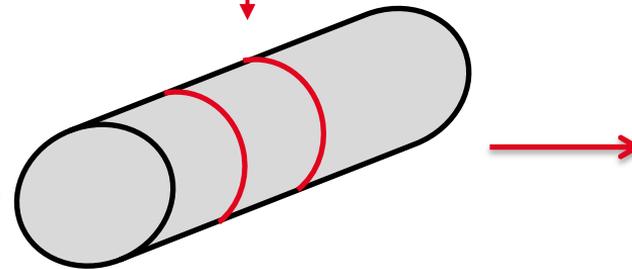
Fluid-loaded cylindrical shell  
*Analytical solution*

Stiffeners and bulkheads  
*Finite Elements Method*

CTF Method



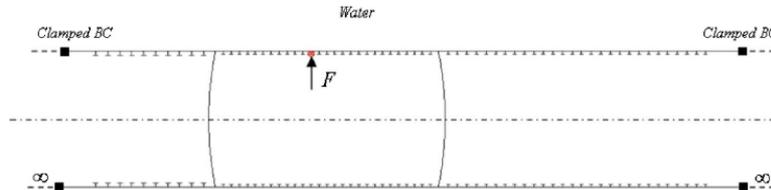
Radial displacements



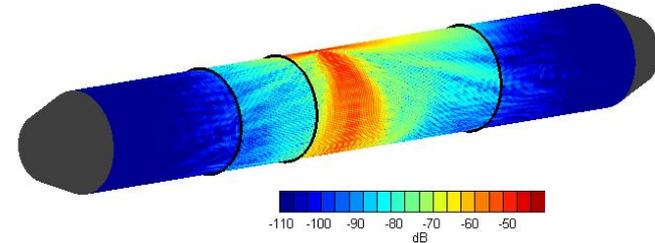
Far-field radiated pressure

# THE CTF METHOD AS AN INDUSTRIAL TOOL

ORCAA: tool developed at Naval Group for vibro-acoustics predictions



Acceleration level (dB) - 3000 Hz - Excited frame n°52



Advantages of the hybrid method:

- Low computation costs compared to FEM/BEM
- Possibility to couple subsystems described by different approaches
- No theoretical frequency limit for the CTF method
- High versatility compared to analytical methods: different stiffeners spacing, various internal structures

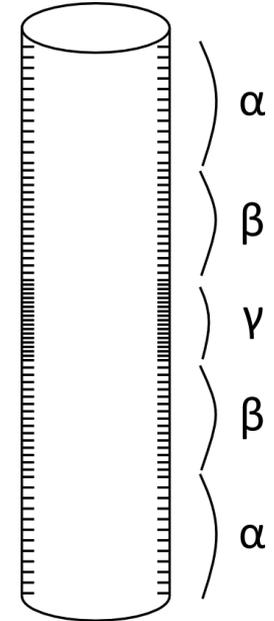
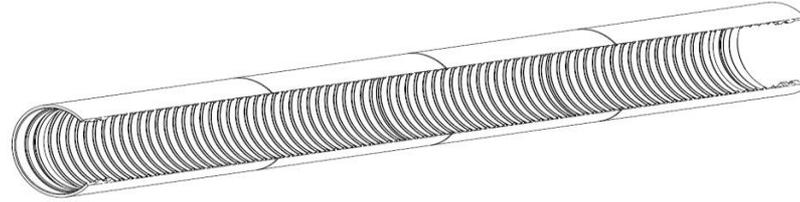
## 2. Experimental work

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# DESCRIPTION OF THE SUBSYSTEMS

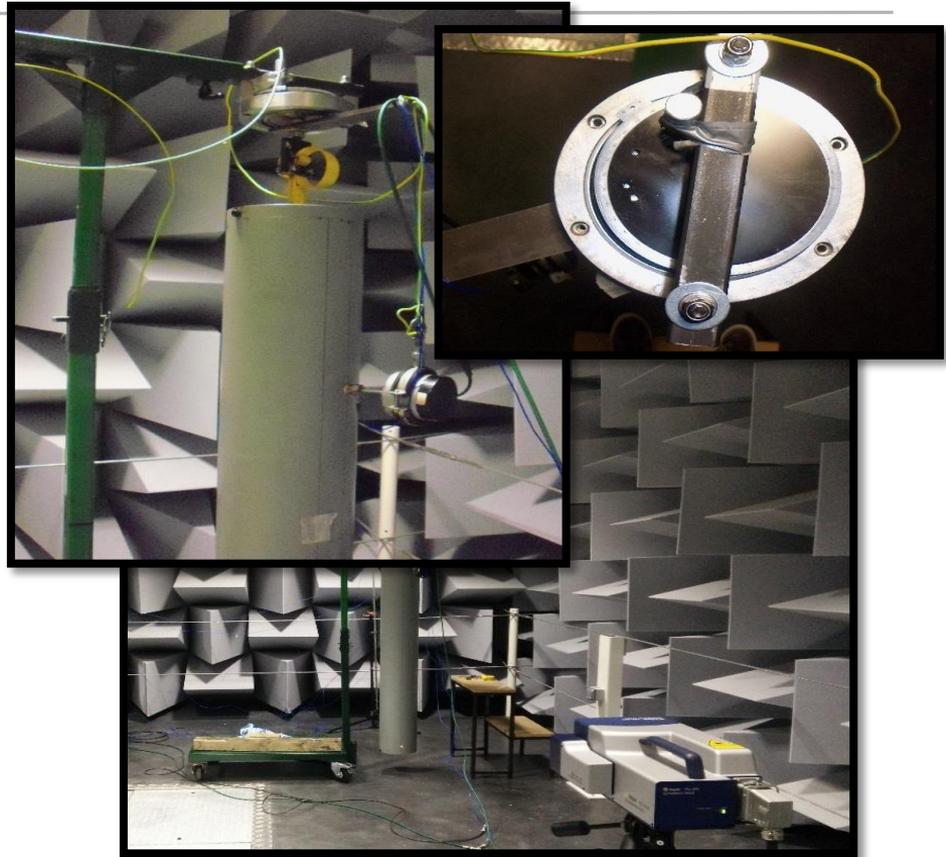
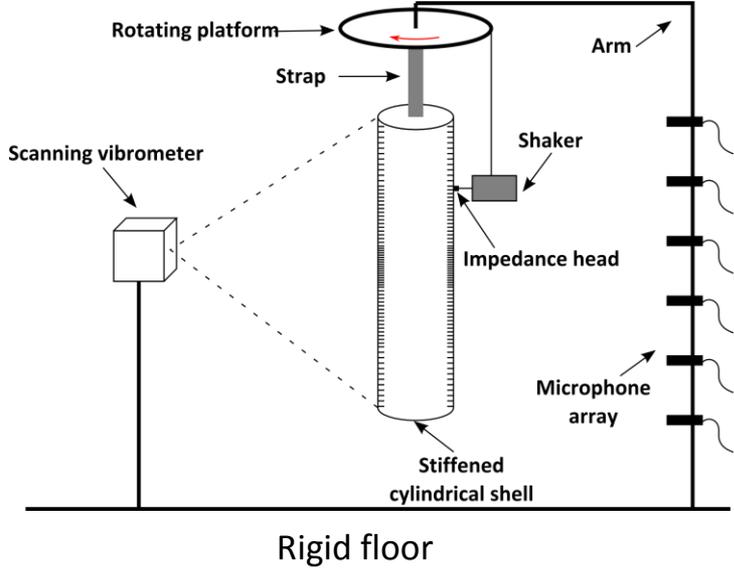
## Stiffened cylinder in steel

- Length: 1,5 m
- Radius: 100 mm
- Thickness: 1,5 mm
- Two end caps
- 3 different stiffeners spacing divided in 5 sections



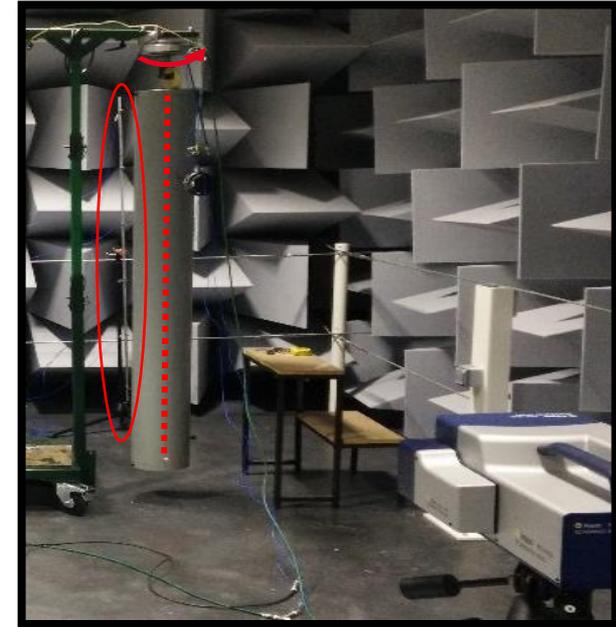
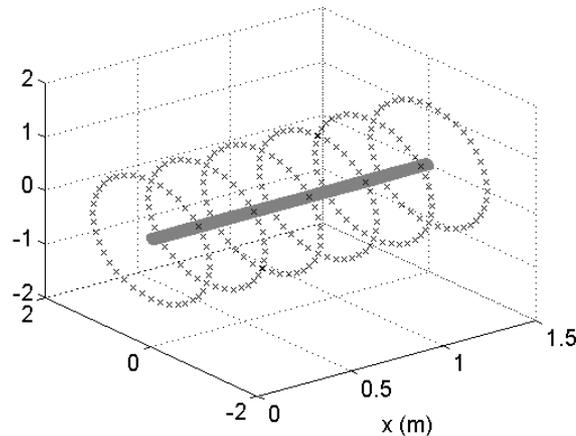
# EXPERIMENTAL SETUP

- In air
- Semi-anechoic room



## DEFINITION OF THE SCANNING GRID

- The maximum distance between two consecutive measurement to capture the physics is 15 mm
- It results in 101 points lengthwise
- Measurement every  $9^\circ$  on half the cylindrical shell (assumption of symmetrical system)
- Microphone array to measure the pressure around the cylindrical shell



## ▼ 3. Results and discussion

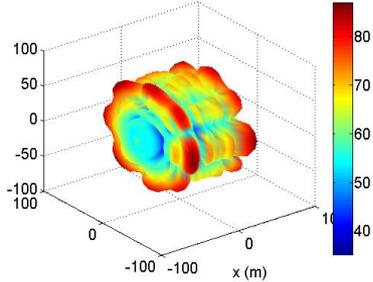
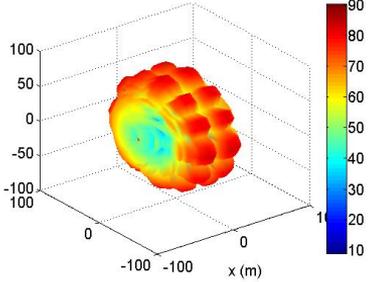
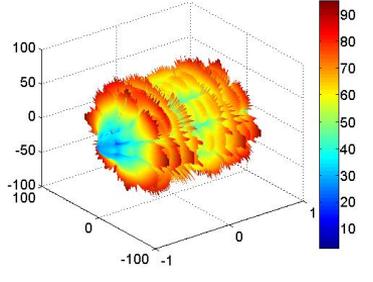
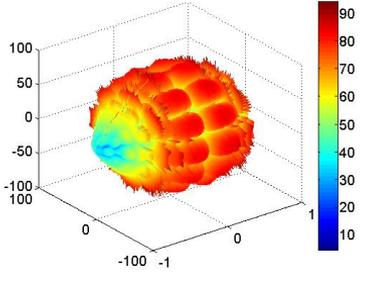
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# MAPS OF RADIAL VELOCITIES

	Global mode $(m,n)=(4,4)$	Local mode
Experimental Work	<p>1980 Hz</p>	<p>3580 Hz</p>
CTF method		

# THE STATIONARY PHASE THEOREM TO CALCULATE THE RADIATED PRESSURE

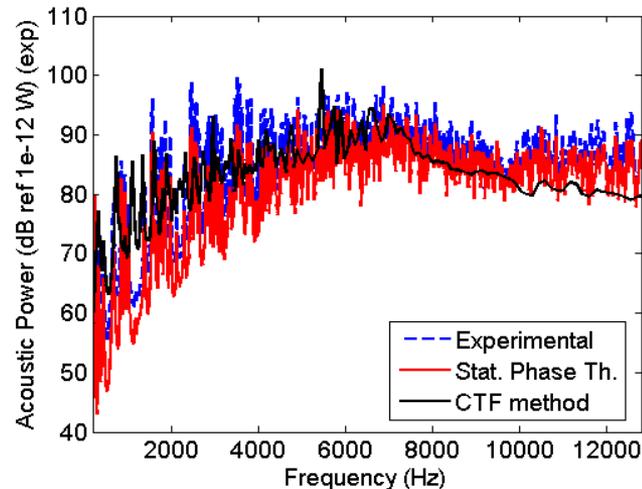
$$p(r, \xi, \theta) = \sum_{n=-\infty}^{+\infty} \frac{2j \rho_0 \omega^2}{r k_0 \cos \xi} \frac{\tilde{W}(-k_0 \sin \xi, n)}{H_n^{(2)'}(R k_0 \cos \xi)} e^{-jrk_0 + jn(\theta + \frac{\pi}{2})}$$

	Global mode $(m,n)=(4,4)$	Local mode
Experimental Work	<p>1980 Hz</p> 	<p>3580 Hz</p> 
CTF method		

# ACOUSTIC POWER RADIATED FROM THE SHELL

Power estimated by 3 means :

- full experimental: summation over the microphone array
- **hybrid**: experimental vibrations + stationnary phase theorem + integral over an enclosing sphere
- full numerical: CTF method + stat. phase th. + integral over an enclosing sphere



## ▼ 4. Summary

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- A numerical method and an experimental procedure have been presented to study the response of a stiffened cylindrical shell
- The vibrations and radiated pressure of a scale model have been measured and calculated and some physical phenomena have been discussed
- Experimental validation of the numerical method

## Perspectives:

- Optimization of the submarine and test new designs to improve acoustic stealth of submarines

NON SENSIBLE

▼  
**Thank you for your attention**

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NAVAL GROUP  
**RESEARCH**

**POWER AT SEA**