

# Digital, Data Analytics, and Automation: Value Creation Through Digital E&P

19-20 NOVEMBER 2024 | BANGKOK, THAILAND



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# Optimizing Waterflood Management in Offshore Field: A Comprehensive Reservoir Management Study Using the Capacitance-Resistance Model (CRM)

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# Agenda

### Part 1: Background and CRM theory

### Part 2: In-house software development: Flood Sight

### Part 3: Field case study on offshore oil field

- Reservoir diagnostics and surveillance
- CRM model analysis and reservoir connectivity
- Reservoir management remedial plan and way forward
- Scenario 1: subblocks with partially-sealed fault
- Scenario 2: subblocks with sandwiched reservoir (aquifer encroachment and gas cap)

### **Results and Conclusions**





### **Problem & Study Objective**



**Secondary and Tertiary recovery mechanism:** Oil is displaced by injected fluids **Lower IOR/EOR performance from brown field development is caused by:** 

- Reservoir complexity
- Poor understanding of inter-well connectivity
- Vertical heterogeneity
- Insufficient production and injection control



- Enable routine use of this analytical workflow by the asset team for continuous optimization.
- Apply the Capacitance-Resistance Model (CRM) along with fundamental reservoir diagnostic for rapid waterflood recovery modeling.
- Integrate fast and effective reservoir management techniques.
- Optimize oil production and minimize bypassed oil in mature oilfields.





### **Background and CRM Theory**

#### Single tank (CRMT)





#### Producer-Injector Pair-based (CRMIP)



Capacitance-Resistance Model (CRM) serves a fast analytical tool designed for modeling waterflood recovery processes, including history match and forecast with optimization.

CRM is a physics-based model, requiring only production, injection and well pressure data to provide information of

 $\tau_i$ 

Ji

- Injection contribution from each injector  $f_{ij}$
- Connected volume for each producer
- Producer productivity index
- Optimized water injection rate

$$q_{j}(t_{k}) = q_{j}(t_{k-1})e^{-\frac{\Delta t_{k}}{\tau_{j}}} + (1 - e^{-\frac{\Delta t_{k}}{\tau_{j}}})(\sum_{i=1}^{N_{i}} f_{ij} i_{i}^{k} - J_{j}\tau_{j} \frac{\Delta P_{wf_{j}}^{(k)}}{\Delta t_{k}})$$
Primary recovery
Fluid injection
Bottomhole pressure
change

 $q_{j,\max}(f_{ij},\tau_j,J_j)$ 

For this study, CRMP will be implemented via the FloodSight software.



# **In-House FloodSight Application**

### Step 1

#### **Input Preparation**

- Historical production rate
- Historical injection rate
- Bottom hole pressure reading
- Well coordinate and well grouping

### Step 2

#### **CRM liquid rate modeling**

- Inter-well connectivity
  - Injection contribution
  - Magnitude and direction
- Reservoir and well property
  - Connected pore volume
  - Productivity
- Liquid rate history matching





### Step 3

Step 4

#### Koval water cut modeling

- Reservoir heterogeneity index
- Water cut modeling
- Oil rate history matching





- No forward activity forecast (NFA)
- Optimized injection scheme
- Estimated waterflood gain
  - Volumetric and profile



 History and forecast
 Forecast with optimization







# Scenario 1: subblocks with partially-sealed fault





- In K-1 reservoir, Block-3: Prod-24 experienced water breakthrough from Inj-11
- In K-1 reservoir, Block-4: No active injector, but GOR of Prod-2 increased when Inj-11's injection dropped, and GOR of Prod-2 decreased after ramping up Inj-11's injection.
- Suspected inter well connectivity between Prod-2 and Inj-11 via a leaky fault, confirmed by pulse testing.
- Group all producers in Blocks 3 and 4 for CRM modeling → need to increase VRR (Inj-11) to maintain waterflood support at Prod-2







# Scenario 1: subblocks with partially-sealed fault





History and forecastForecast with optimization











# Scenario 2: subblocks with sandwiched reservoir





- In K-3 reservoir, Block-1: Prod-14 experienced water breakthrough from Inj-7
- Prod-13 experienced high GOR due to gas cap expansion, with insufficient pressure support from Inj-7. Waterflood response at Prod-13 is blocked by Prod-14.
- Calculate instantaneous VRR (iVRR)

$$q_{L} (Prod-13) = 570 BBL/D, WCT < 0.1\%$$

$$q_{L} (Prod-14) = 1,500 BBL/D, WCT = 72\%$$

$$q_{inj} (Inj-7) = 1,190 BBL/D$$

$$iVRR = \frac{\sum q_{inj}B_{w}}{\sum (q_{o}B_{o} + q_{w}B_{w})}$$

$$= \frac{1190 \times 1}{1500 \times 0.72 + [1500 \times 0.28 \times 1.3 + 570 \times 1.3]} = 0.5$$

Set iVRR = 1 and fix q<sub>inj</sub> (Inj-7) at 1,190 BBL/D

 cut back gross at Prod-14 since it already sees high water cut and divert water to Prod-13

q <sub>inj</sub> (Inj-7)	$q_L$ (Prod-13)	$q_L$ (Prod-14)	iVRR
1,190	570	1,500	0.5
1,190	743	207 🖊	1.0





# Scenario 2: subblocks with sandwiched reservoir





History and forecast

Forecast with optimization

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### **Results and Conclusions**





#### Key deliverables: New water injection requirement

- New injection requirement is proposed by CRM optimizer.
- For scenario 1, increase **injection rate to boost oil production** in the adjacent subblocks with transmissible faults.
- For scenario 2, cut gross rate at high water-cut producer to avoid water recycling and support waterflood to more updip wells.

#### **Conclusions and Key take aways**

- Field water injection rate remains at 20,000 BBL/D but gets redistributed among injectors to maximize oil gain.
- Repeat CRM workflow for all subblocks → Oil Gain + 1.3 MMSTB
- This study examines the implementation of the PTTEP in-house capacitanceresistance model, Floodsight, The incorporation of the CRM model is recommended due to its speed, repeatability, and low computational resource requirement.