



Society of Petroleum Engineers



# Gas Field Development and Production – State of Play

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# Analytical Model for Well Injectivity Prediction on CO<sub>2</sub> Injection in Heterogeneous Reservoirs

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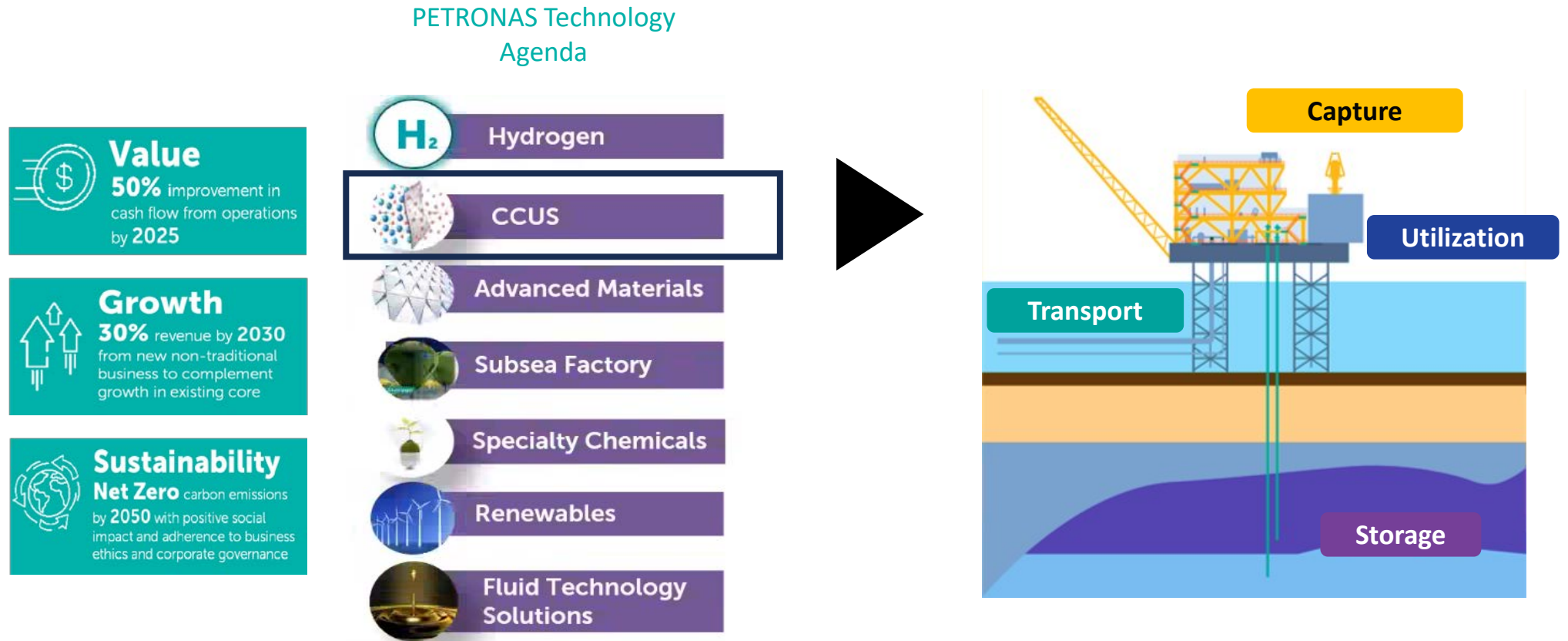
<sup>2</sup>The University of Adelaide



# Outline

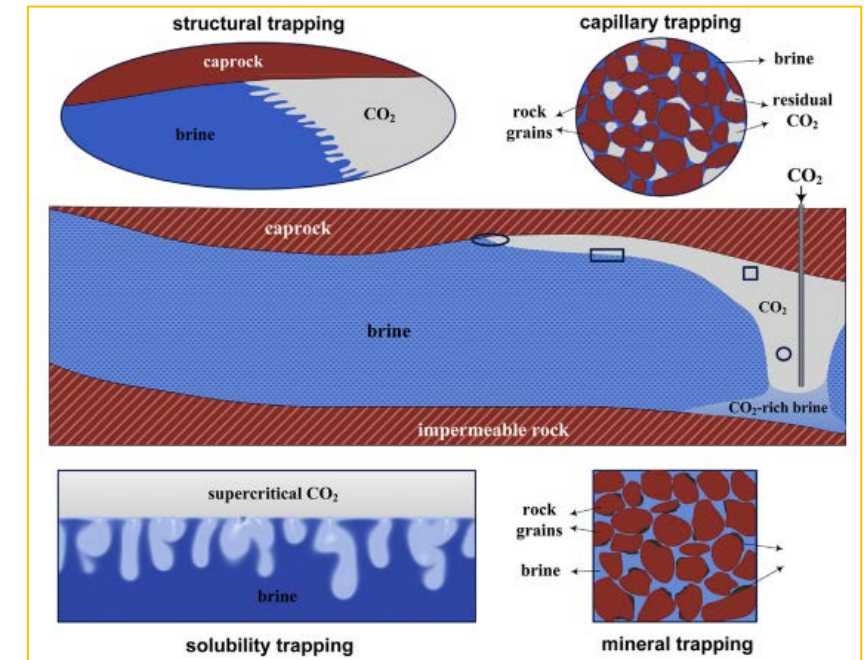
- Overview – Carbon capture and storage (CCS)
- Factor causes CO<sub>2</sub> injectivity declines
- Development of analytical model – workflow
- Expression of well impedance during CO<sub>2</sub> injections
- New analytical formulae for well impedance
- Results
- Summary
- Conclusions
- Acknowledgements

# Positioning to future new normal, refresh Technology Agenda is imminent to deliver MFT 50.30.0 and supporting future growth areas for PETRONAS



# Overview - Carbon capture and storage (CCS)

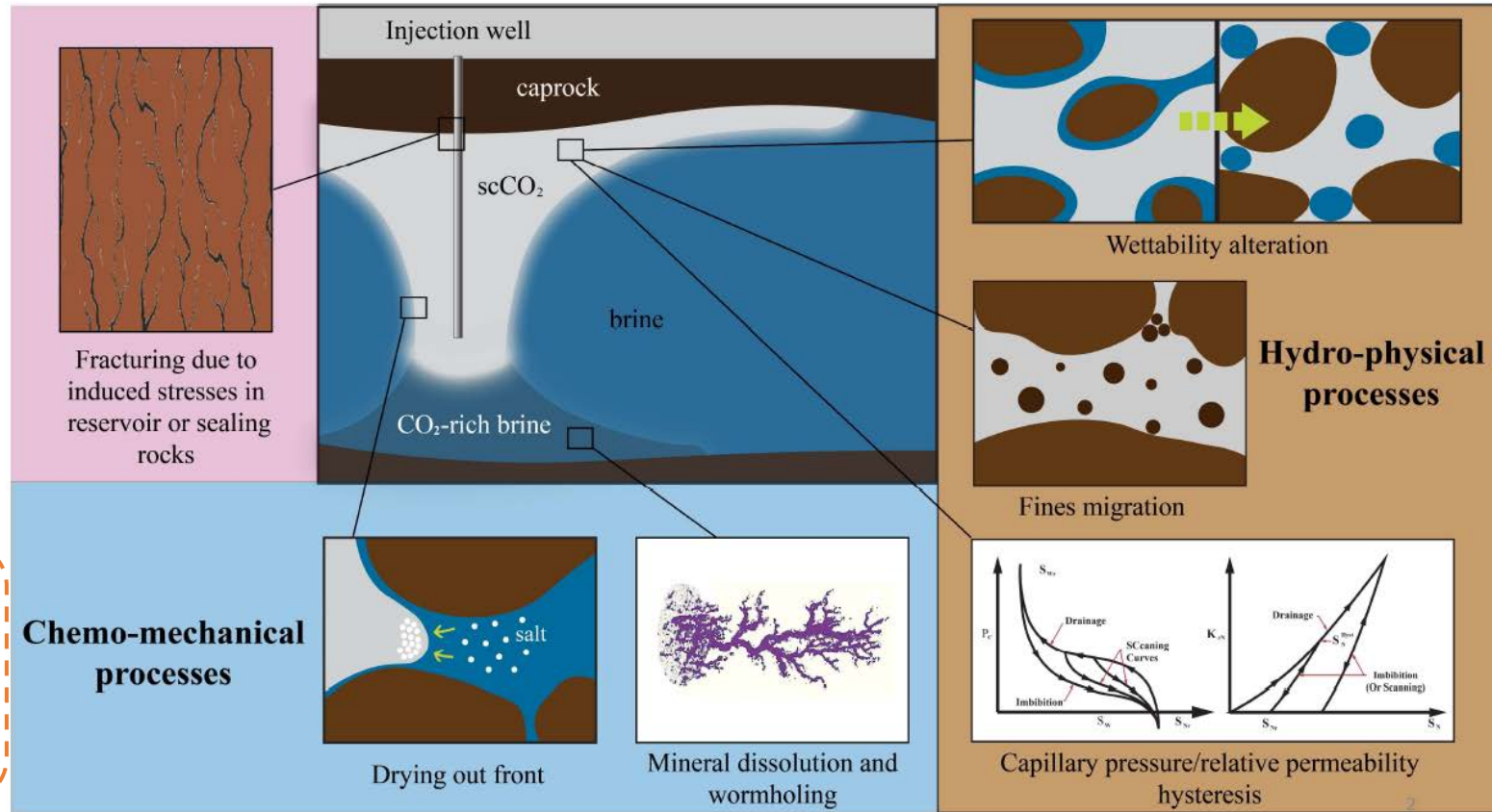
- CCS - process that involves capturing the CO<sub>2</sub> at its source & storing it permanently subsurface
- PETRONAS is currently embarking an opportunity for CO<sub>2</sub> storage at oil & gas reservoir and deep saline aquifer for short- and long-term geo-sequestration
- However, CO<sub>2</sub> storage into aquifers has greater complexity, as it causes various hydro-physical, chemical, and geomechanical interactions that affect the injectivity of wellbores



CO<sub>2</sub> trapping mechanism



# Factor causes CO<sub>2</sub> injectivity declines



Lost of seal/caprock integrity

Salt precipitation by Joule-Thompson (JT) cooling down and water evaporation into CO<sub>2</sub>

Chemo-mechanical processes

Drying out front

Mineral dissolution and wormholing

Wettability alteration

Hydro-physical processes

Fines migration

Capillary pressure/relative permeability hysteresis

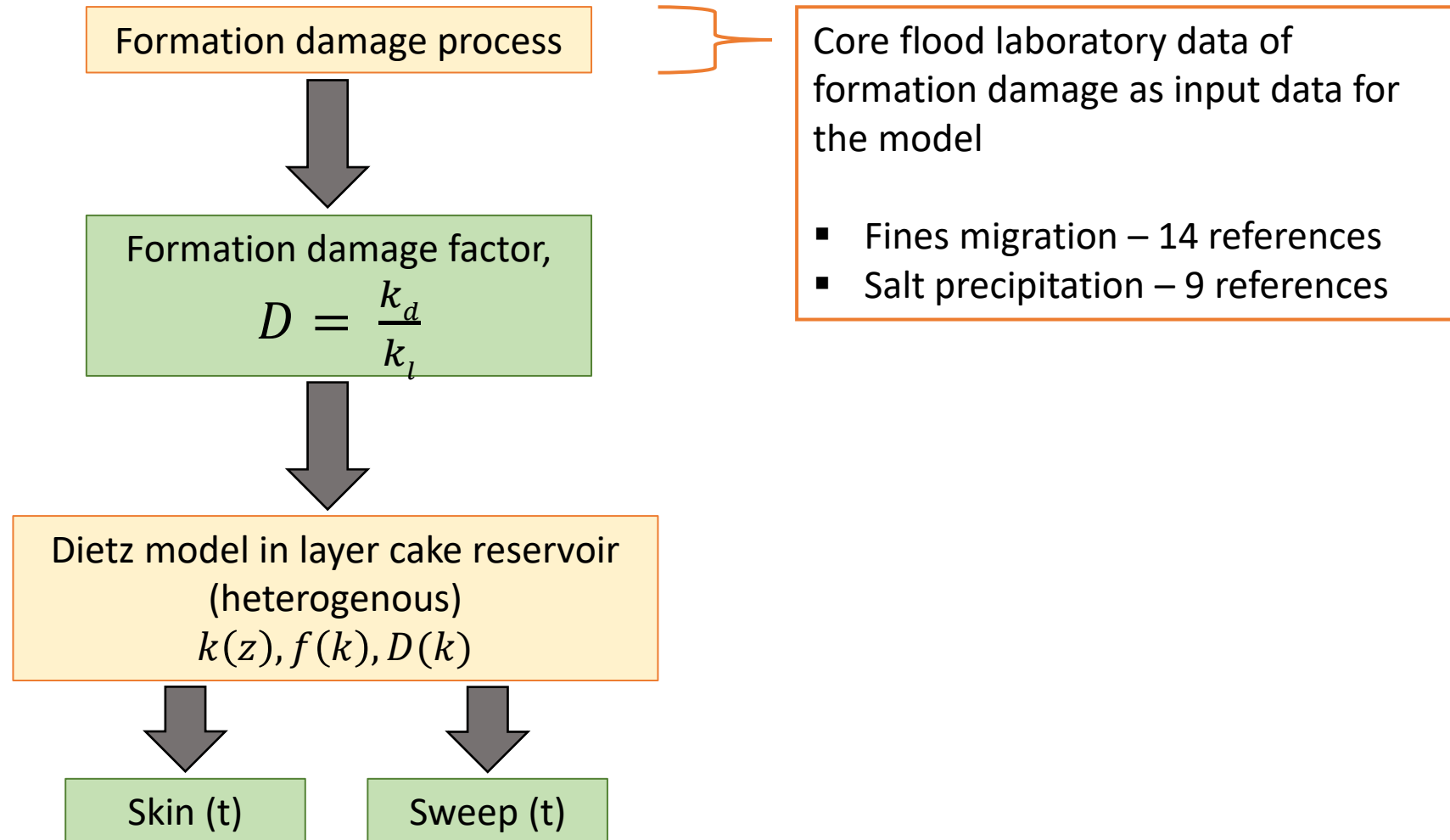
Wettability alteration

Fines mobilization and migration by water evaporation into CO<sub>2</sub>

Effects of water-CO<sub>2</sub> wettability on relative permeability and capillary pressure

Dissolution of rock in carbonic acid with release of solid particles

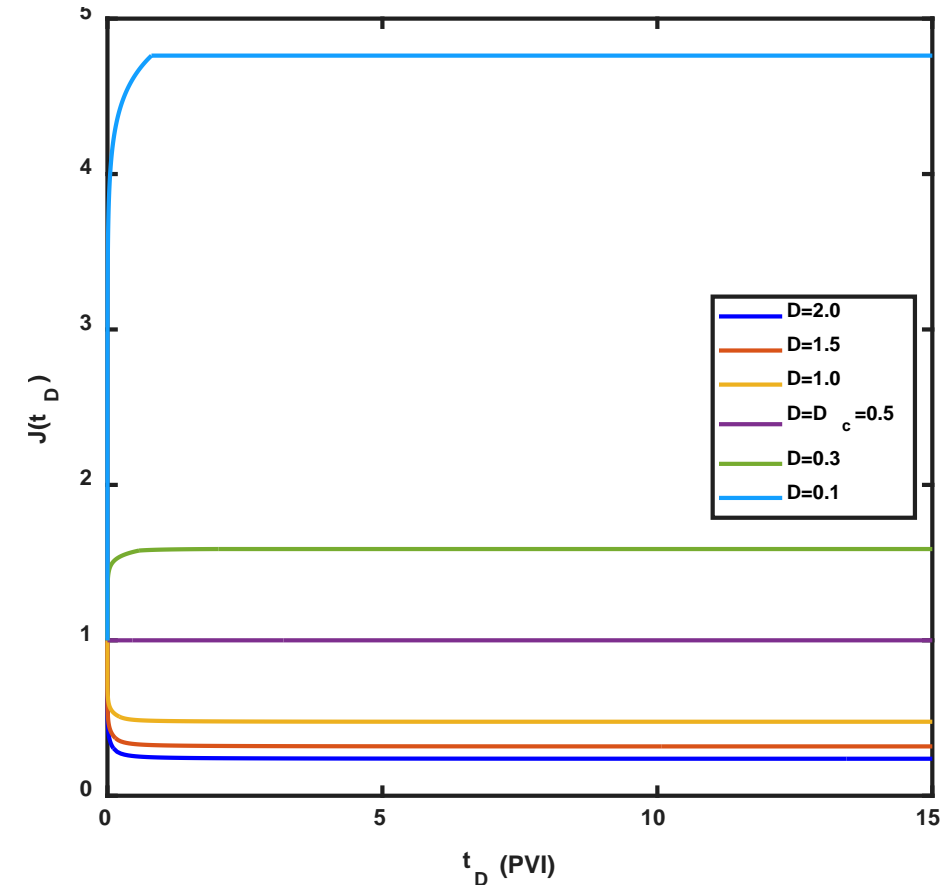
# Workflow for Development of analytical model



# Expression of well impedance during CO<sub>2</sub> injections

Formation damage  
governing equations

$$J(t_D) = \frac{II(t_D = 0)}{II(t_D)} = \frac{q(t_D = 0) \Delta p(t_D)}{\Delta p(t_D = 0) q(t_D)}$$



Well impedance versus dimensionless time at different damage ratios for  $c=0.5$  in power-law profile



# New analytical formulae for well impedance

$$J(t) = \begin{cases} \frac{\mu_g \ln\left(\frac{D_i t + x_w}{x_w}\right)}{\mu_w k_{rgwi} D \langle k \rangle} + \int_{s_{wi}}^{s_f} \frac{f''(s)}{\left(f'(s) + \frac{x_w}{t}\right) \Lambda(s)} ds - \frac{\ln(D_f t + x_w)}{\langle k \rangle} & 0 < t < \frac{1 - x_w}{D_f} \\ \frac{\mu_g \ln\left(\frac{D_i t + x_w}{x_w}\right)}{\mu_w k_{rgwi} D \langle k \rangle} + \int_{s_{wi}}^{s_t} \frac{f''(s)}{\left(f'(s) + \frac{x_w}{t}\right) \Lambda(s)} ds & \frac{1 - x_w}{D_f} < t < \frac{1 - x_w}{D_i} \\ -\frac{\mu_g \ln(x_w)}{\mu_w k_{rgwi} D \langle k \rangle} & \frac{1 - x_w}{D_i} < t < \infty \end{cases}$$

The impedance, J is determined by pressure losses

- (i) near to well (early time)
- (ii) in mixture zone (after breakthrough)
- (iii) in water zone (late time)

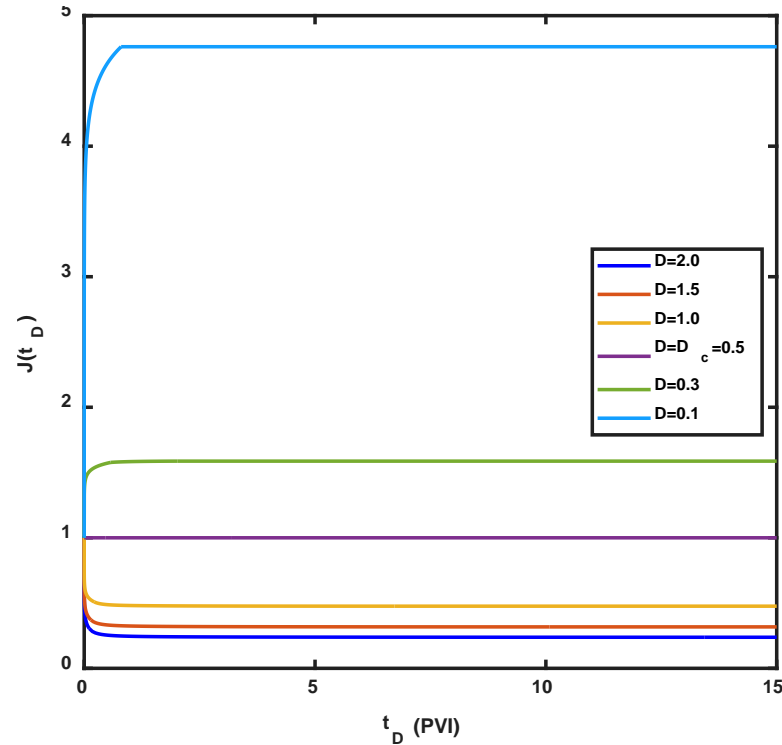
Field data:  $k(z)$  or  $g(k)$  – permeability distribution;  $\text{CO}_2$  and water viscosities;

Lab data: D is the ratio between the damaged and initial permeabilities

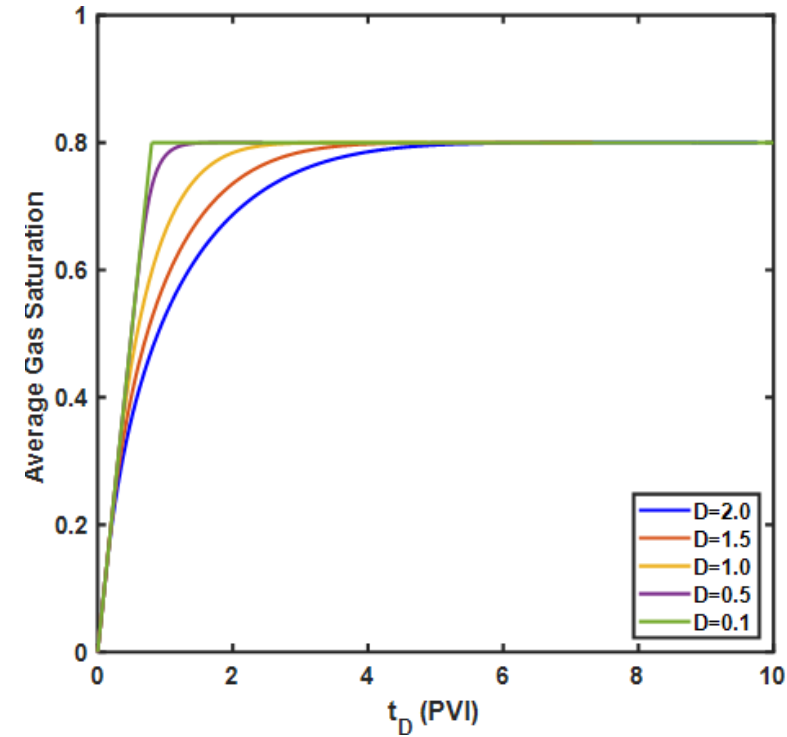


Introduced analytical model for 2 phase flow with formation damage

# Sweep coefficient evolution



Well impedance versus dimensionless time at different damage ratios for  $c=0.5$  in power-law profile



The higher is the induced formation damage,  $D$  the higher the well impedance,  $J$  and skin factor,  $S$  of the injection well, and the higher the sweep coefficient

# Results (1/2)

## Application of analytical modelling for sweep efficiency and well index calculation

### Case study Field LW

#### Field overview

- Shallow offshore (60 m water depth)
- Depleted gas reservoir with weak aquifer support (21 production wells)
- Reservoir gas – 13% CO<sub>2</sub>
- Depositional environment – shallow marine clastic

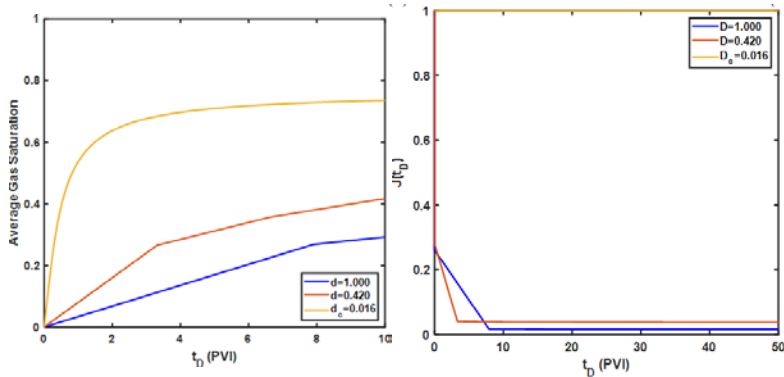
Reservoirs	E-20/25	E-40/45/50	D-32/36
Reservoir temperature (°F)	235	250-260	214
Latest average reservoir pressure (psia)	600	800	700
<b>Statistical parameters for permeability histograms</b>			
Minimum	0	0	0
Maximum	2450	995	4000
Mean	72.30	64.28	320.18
Standard Deviation	235.15	116.89	504.80
Skewness	8.69	3.71	2.42
Kurtosis	86.87	20.28	8.89

# Results (2/2)

Application of analytical modelling for sweep efficiency and well index calculation

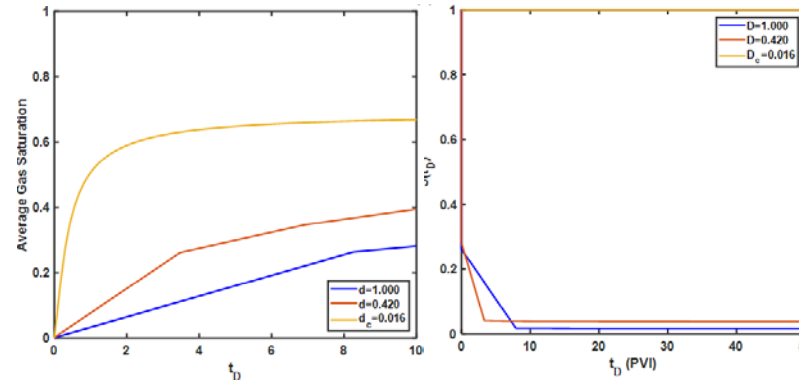
Well impedance versus dimensionless time when damage factor changes from 1 to critical value 0.016

E-20/25



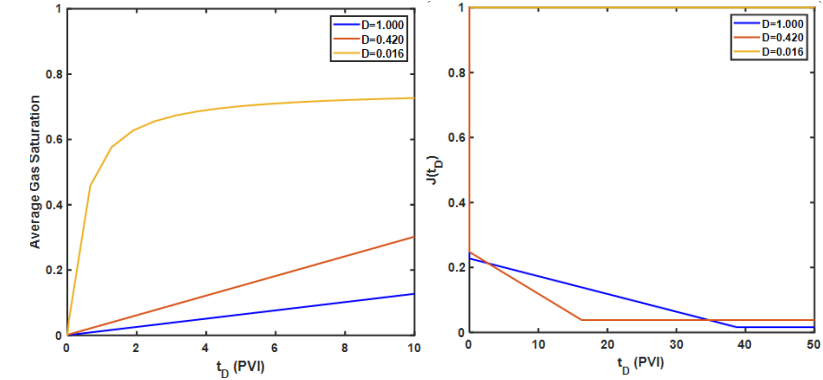
Sweep increases from 3 % to 53% and impedance increases from 0.23 to 1

E-40/45/50



Sweep increases from 7% to 50% and impedance increases from 0.20 to 1

D-32/36



Sweep increases from 1% to 52% and impedance increases from 0.22 to 1

# Summary

- The analytical model allows derivation of the explicit formulae for well impedance / skin factor and sweep coefficient evolution during formation damage accumulation induced by CO<sub>2</sub> injection
- The higher is the induced formation damage, the higher the well impedance and skin factor of the injection well, and the higher the sweep coefficient due to creation of additional hydraulic resistance to the injected gas. So, formation damage increases gas storage capacity of the geological formation

## Conclusion

The analytical model for CO<sub>2</sub> injection in heterogenous with inter-layer communications for prediction of well injectivity and the reservoir sweep efficiency will guide the decision making for an effective CCS projects because formation damage not only makes it difficult to inject, at the same time increases the storage capacity



# Acknowledgements

PETRONAS Research Sdn Bhd

PETRONAS Carigali Sdn Bhd

The University of Adelaide



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**THANK YOU**

# Development of analytical model - general

The analytical model allows derivation of the explicit formulae for well impedance / skin factor and sweep coefficient evolution during formation damage accumulation induced by CO<sub>2</sub> injection

1. General model for injectivity decline during CO<sub>2</sub> injection into layer-cake reservoir

2. Sweep enhancement by induced formation damage

3. Well-reservoir interaction

4. Analytical model for Joule-Thompson cooling due to CO<sub>2</sub>

5. Analytical model for water evaporation into injected CO<sub>2</sub>

6. Analytical model for fines mobilisation and straining during displacement of water by CO<sub>2</sub>

7. Simultaneous determination of relative permeability and capillary pressure for brine-CO<sub>2</sub> by a novel steady-state-transition test (SSTT)